Correction

APPLIED PHYSICAL SCIENCES, PLANT BIOLOGY

Correction for “Universal poroelastic mechanism for hydraulic signals in biomimetic and natural branches,” by J.-F. Louf, G. Guéna, E. Badel, and Y. Forterre, which was first published October 2, 2017; 10.1073/pnas.1707675114 (*Proc Natl Acad Sci USA* 114:11034–11039).

The authors note that, due to a printer’s error, the affiliation for E. Badel should instead appear as Université Clermont Auvergne, INRA, PIAF, F-63000 Clermont-Ferrand, France. The corrected author and affiliation lines appear below. The online version has been corrected.

J.-F. Louf[a], G. Guéna[a], E. Badel[b], and Y. Forterre[a]

[a]Aix-Marseille Univ, CNRS, IUSTI (Institut Universitaire des Systèmes Thermiques Industriels), 13013 Marseille, France; and [b]Université Clermont Auvergne, INRA, PIAF, F-63000 Clermont-Ferrand, France

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Universal poroelastic mechanism for hydraulic signals in biomimetic and natural branches

J.-F. Louf[a], G. Guéna[a], E. Badel[b], and Y. Forterre[a,1]

[a]Aix-Marseille Univ, CNRS, IUSTI (Institut Universitaire des Systèmes Thermiques Industriels), 13013 Marseille, France; and [b]Université Clermont Auvergne, INRA, PIAF, F-63000 Clermont-Ferrand, France

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Plants constantly undergo external mechanical loads such as wind or touch and respond to these stimuli by acclimating their growth processes. A fascinating feature of this mechanical-induced growth response is that it can occur rapidly and at long distance from the initial site of stimulation, suggesting the existence of a fast signal that propagates across the whole plant. The nature and origin of the signal is still not understood, but it has been recently suggested that it could be purely mechanical and originate from the coupling between the local deformation of the tissues (bending) and the water pressure in the plant vascular system. Here, we address the physical origin of this hydromechanical coupling using a biomimetic strategy. We designed soft artificial branches perforated with longitudinal liquid-filled channels that mimic the basic features of natural stems and branches. In response to bending, a strong overpressure is generated in the channels that varies quadratically with the bending curvature. A model based on a mechanism analogous to the ovalization of hollow tubes enables us to predict quantitatively this nonlinear poroelastic response and identify the key physical parameters that control the generation of the pressure pulse. Further experiments conducted on natural tree branches reveal the same phenomenology. Once rescaled by the model prediction, both the biomimetic and natural branches fall on the same master curve, enlightening the universality of our poroelastic mechanism for the generation of hydraulic signals in plants.

plant biomechanics | biomimetism | long-distance signaling | poroelasticity | nonlinear beams

Since Darwin and Knight (1, 2), scientists have known that plants are able to perceive external mechanical perturbation and respond to these stimuli by modifying their growth, a process called thigmomorphogenesis (3–6). In response to mechanical stress, plants tend to decrease their elongation growth and, for plants having secondary growth like trees, increase the diameter of their organs. Over the past decades, reports have refined our understanding of thigmomorphogenesis at the biomechanical, physiological, and molecular levels (4, 7–12). A remarkable feature of this mechanically induced response is that it can be local and also nonlocal. When a shoot is bent, a sudden arrest of the elongation growth is observed far away from the perturbed area (13) within minutes (8). These experiments demonstrate that plants can carry mechanosensing information over a long distance (from centimeters to meters) very rapidly throughout the whole organ. Among the different hypotheses for this long-distance signaling [hormones transport and electrical signals (14–16)], it has long been argued that hydraulic pulses could provide a unique way for rapid communication in plants, thanks to their highly connected hydraulic network that brings water from the roots to the leaves (16–18). Propagating hydraulic waves were first mentioned by Ricca in the 1920s during his study of the sensitive plant *Mimosa pudica* (19) and later observed in different organisms in response to wounding stress, often in association with electrical waves of depolarization (20–22). Recently, Lopez et al. (23) observed that bending the stem of a whole living tree or an isolated branch segment generates a sudden overpressure that propagates rapidly in the plant vascular system. This hydraulic signal induced by a nonwounding elastic stress appears as a promising candidate for the rapid communication of the thigmomorphogenetic response. However, the physical mechanisms responsible for its generation and the parameters that govern its properties remain poorly understood. In mechanics, the hydraulic response of a porous material saturated with water, like a branch or a stem, is described by the poroelastic theory (24, 25). In this framework, the bending of a branch is expected to induce local water expulsion/suction in response to the longitudinal compression/tension strains of the plant tissues from both sides of the neutral surface of the branch. However, according to the linear beam theory, these local changes of volume should cancel each other out in average over the whole system. Therefore, it remains unclear how hydraulic signals could be generated in plants from such bending stress.

The objective of this study is to understand the origin of this hydromechanical coupling and the physical parameters that control the generation of hydraulic pulses induced by bending in plant tissues. To this end, we use a biomimetic approach (26–29) and study the hydraulic response to bending of soft artificial branches that mimic the basic structural and mechanical features of natural stems and branches. While previous theoretical and experimental works have studied the linear behavior of poroelastic beams (30–32), very few have investigated the large deformation regime of fluid-infiltrated media composed of cellular materials like wood or soft plant tissues (33). In this work, we

Significance

Plants are sessile organisms without nerves. As such, they have developed specific mechanisms to carry information rapidly throughout their body in response to mechanical stimuli. Recently, it has been suggested that the first stage of this long-distance signaling could be the propagation of hydraulic signals induced by the mechanical deformation of the plant tissue (bending), but the physical origin of this hydromechanical coupling remains a conundrum. Here, we address this issue by combining experiments on natural tree branches and soft biomimetic beams with modeling. We reveal a generic nonlinear mechanism responsible for the generation of hydraulic pulses induced by bending in poroelastic branches. Our study gives a physical basis for long-distance communication in plants based on fast hydraulic signals.

Author contributions: J.-F.L., G.G., E.B., and Y.F. designed research, performed research, analyzed data, and wrote the paper.

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[1] To whom correspondence should be addressed. Email: yoel.forterre@univ-amu.fr.

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demonstrate a generic nonlinear mechanism responsible for the generation of hydraulic pulses in both biomimetic and natural tree branches representative of wood diversity.

Results

Evidence of Hydraulic Pulses Induced by Bending in Soft Biomimetic Branches. From a mechanical perspective, tree branches and stems can be viewed in first approximation as flexible elastic beams composed of microchannels that carry water longitudinally (34, 35) (Fig. 1*A*). To mimic these minimal ingredients, we use polydimethylsiloxane (PDMS)-based 3D molding techniques to design soft synthetic branches (Young modulus $E\sim 0.1-1$ MPa, radius $R=5$ mm, length $L=100$ mm) perforated with parallel longitudinal microchannels (diameter $d=500$ µm) with various channel numbers and array patterns (Fig. 1 *B* and *C* and *Materials and Methods*). The channels are filled with a nonvolatile liquid (silicone oil) and connected together to a pressure sensor at one extremity of the beam, while the other extremity is closed (Fig. 2*A*). To bend the branch, we design an original setup in which one extremity of the beam is fixed and the other is moved by using a system of pivoting arms connected to a linear displacement motor (Fig. 2*B*, *Bending Setup for the Biomimetic Branches*, and Fig. S1). This enables us to apply a uniform curvature on the soft beam, while minimizing compressional and shearing effects within the material. The bending strain ε_B is then defined as the maximal longitudinal strain in the beam: $\varepsilon_B=\overline{C}R$ (36), where $\overline{C}$ is the mean curvature measured by image analysis.

A typical pressure response of the synthetic branch for a bending strain ε_B of order 10% is shown in Fig. 2*C*. Here, the beam is initially straight, and the internal fluid pressure in the channels is equal to the atmospheric pressure $P_{\mathrm{ref}}=P_0$ (no effect of the initial pressure is noticed as long as $|P_{\mathrm{ref}}-P_0|$ is small compared with the beam Young's modulus E). In response to bending, a mean overpressure rises up inside the channels and reaches a steady value ΔP of the order of a few kilopascals. When the branch is brought back to its initial straight shape, the overpressure goes back to zero, showing the reversible nature of this hydraulic response. The striking observation is that the overpressure strongly increases with the bending strain, with a quadratic relationship $\Delta P\propto\varepsilon_B^2$ that is independent of the bending protocol (Fig. 2*D*). This nonlinearity does not come from the intrinsic material properties, since the maximal strain in our case ($\varepsilon_B\sim 0.1-0.2$) is far below the linear elastic limit of the PDMS elastomer ($\varepsilon\sim 1$). Experiments with beams of different Young's modulus E and channel geometries all exhibit the quadratic relationship between the pressure and the bending strain (Fig. 2*E*). The response appears independent of the channels' number or distribution, but strongly increases with the beam's rigidity. This confirms that the generation of these hydraulic pulses arises from a purely elastic phenomenon.

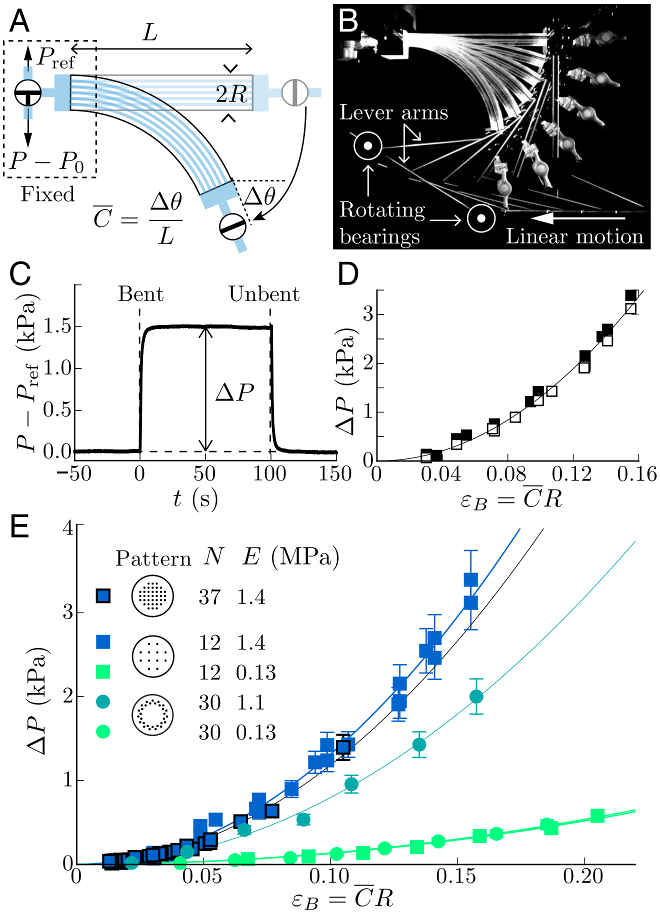

Fig. 2. Hydraulic pulse induced by bending in PDMS biomimetic branches. (*A* and *B*) Sketch (*A*) and picture (*B*) of the bending setup and pressure measurements, where $\Delta\theta$ is the variation of angle between the free extremity and the clamped extremity of the beam, $\overline{C}$ the mean curvature of the beam, R the beam radius, P_{ref} is the initial fluid-pressure in the channels, and $P-P_0$ is the fluid-pressure in the channels relative to the atmospheric pressure. (*C*) Pressure response to bending/unbending sequence in a closed system (square channel pattern, $N=12$, $E=1.4$ MPa, $\varepsilon_B=\overline{C}R\simeq 0.1$). (*D*) Steady overpressure ΔP vs. bending strain $\varepsilon_B=\overline{C}R$. Filled square, bent/unbent cycles with return to the straight state; open square, positive ramp of strain. (*E*) Overpressure ΔP vs. bending strain ε_B for various channel patterns, number of channels N, and PDMS Young moduli E. The solid lines in *D* and *E* are quadratic fits of the data.

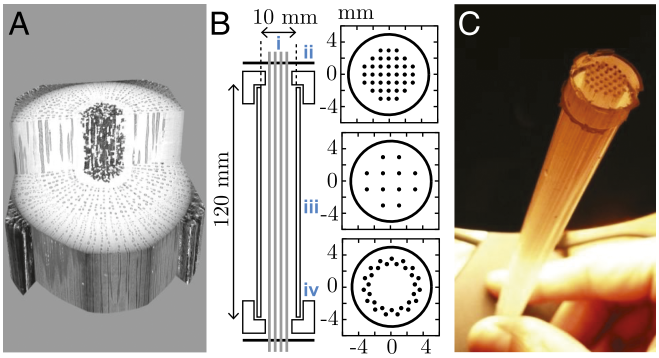

Fig. 1. Natural vs. biomimetic tree branches. (*A*) X-ray microtomography of a *Vitis vinifera* branch (grape vine), showing the network of longitudinal conducting vessels (dark gray). (*B*) Sketch of the mold used to design the synthetic branch with the different channel patterns investigated (*Top*, square array, $N=37$; *Middle*, square array, $N=12$; *Bottom*, circular array, $N=30$): *i*, piano strings; *ii*, POM plate; *iii*, Plexiglas tube; *iv*, Plexiglas block. (*C*) Picture of the synthetic branch made of PDMS elastomer after removal from the mold (*Materials and Methods*).

Physical Modeling: A Nonlinear Poroelastic Coupling. Our biomimetic system therefore contains the relevant physical ingredients needed to reproduce the hydraulic pulse induced by bending recently reported in plant tissues (23). However, explaining the generation of this pulse is not straightforward. Classical linear beam theory tells us that the total volume of a symmetrical bent beam should remain constant, regardless of its elastic properties (36). This would predict a null pressure variation in a closed poroelastic beam with interconnected channels, in contradiction with observations.

To solve this paradox, we propose a nonlinear mechanism analogous to the ovalization of thin elastic tubes (37). When an elastic beam is bent, the longitudinal elastic strain (extension or compression) increases linearly with the distance to the neutral surface (Fig. 3 *A*, *Left*). This induces a bending elastic energy per unit volume that varies quadratically with the radius of the beam, $U_b \sim E\varepsilon_B^2 \sim EC^2R^2$, where E is the beam Young's modulus and C is the bending curvature, assumed uniform here (36). Therefore, a way for the system to lower the bending elastic energy is to squeeze its cross-section, hence decreasing the beam radius by a quantity δ in the transverse direction (Fig. 3 *A*, *Right*). The maximal bending strain then reduces to $C(R-\delta)$ and the bending energy to $U_b \sim EC^2(R-\delta)^2$. However, this transverse compression δ/R involves the cost of a positive compressive energy in the transverse direction $U_c \sim E(\delta/R)^2$. By minimizing the sum of the bending and compressive elastic energy, $\frac{d}{d\delta}(U_b + U_c) = 0$, the transverse compression is found to vary quadratically with the bending longitudinal strain: $\delta/R \sim \varepsilon_B^2$. For an elastic beam perforated with longitudinal channels, this compression is associated with a reduction of the channels' volume $\Delta V_c/V_c \sim -\delta/R$, where V_c is the total volume of the channels (38). If now the channels are filled with an incompressible liquid and closed, this reduction in volume is converted into a global rise of pore pressure $\Delta P = -B\Delta V_c/V_c$, such that:

$$\Delta P = \gamma B \varepsilon_B^2. \qquad [1]$$

The coefficient B, which relates the variation of liquid volume in the channels to the change of pore pressure, is an elastic bulk modulus known as the inverse of the specific storage coefficient in the poroelastic literature (39). Dimensionally, B is proportional to the beam Young's modulus E and depends on the channels' distribution and geometry. The dimensionless factor reads $\gamma = 1/2$ in the framework of this simple energy model, which assumes a uniform transverse compression (see *Energy Model for Anisotropic Beams*). A more elaborate model shows that the transverse compression is actually nonuniform and maximal at the neutral line (*Materials and Methods*, Eq. **2**). As a result, γ is found to weakly depend on the channels' distribution and varies between 0.56 and 0.59 for our biomimetic beams (*Materials and Methods*, Eq. **4**).

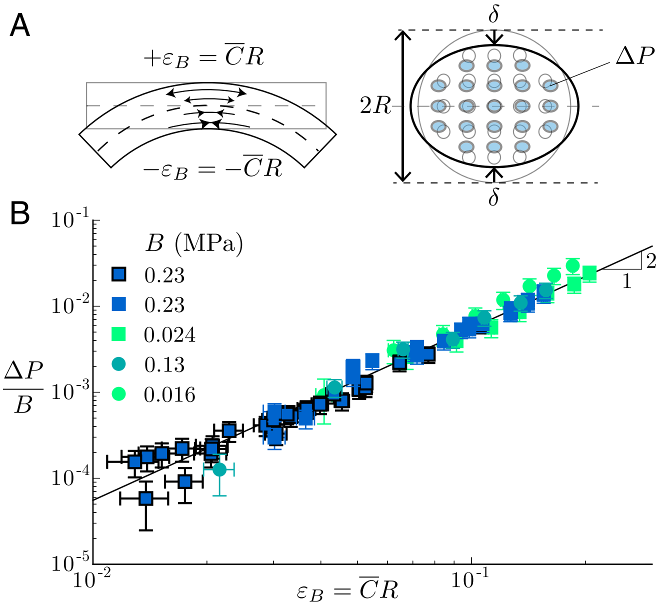

Fig. 3. Mechanism of hydraulic pulse generation and poroelastic modeling. (*A*) The nonlinear coupling between bending and transverse modes of deformation induces a transversal squeezing of the branch's channels $\delta/R \propto \varepsilon_B^2$ and thus an overpressure in the channels varying as $\Delta P \propto B\varepsilon_B^2$, where B is the elastic bulk modulus of the branch. (*B*) Overpressure ΔP normalized by the measured elastic bulk modulus B as a function of the bending deformation ε_B for all biomimetic branches studied (same symbols as in Fig. 2*E*). The solid line gives the best quadratic fit of the data in log–log scale: $\Delta P/B = (0.55 \pm 0.02) \times \varepsilon_B^2$ ($R^2 = 0.972$).

Our model therefore predicts that the bending of poroelastic beams filled with a liquid generates a global increase of the pressure that varies quadratically with the bending strain, as observed experimentally. To test Eq. **1**, we independently measure the elastic bulk modulus B of the biomimetic branches (*Materials and Methods*, Eq. **2**). As predicted, data for various Young's modulus and channel geometry all collapse into a single curve of slope 2 in log–log scale when overpressure is normalized by the bulk modulus B (Fig. 3*B*). The prefactor γ found experimentally (0.55 ± 0.02) agrees with the prediction of the model, showing the relevance of the nonlinear mechanism we propose for the generation of hydraulic pulses in the biomimetic porous branches (see *Influence of the Bending Mode on the Pressure Response* and Fig. S2 for additional comparison with the model in the case of a nonuniform curvature).

Experiments on Natural Woody Branches. To check the validity of the model in the context of plants, we conduct experiments on natural tree branches and stems (*Materials and Methods* and *Plant Materials*). Three species representative of the wood anatomy diversity are studied: a gymnosperm species (*P. sylvestris* L.), whose conducting hydraulic network is made of tiny and short conduits (tracheids) regularly distributed; a ring porous angiosperm species (*Quercus ilex* L.), where the large conducting vessels are concentrated in the earlywood zone; and a diffuse porous angiosperm species (*P. alba* × *tremula* L. clone 717-1B4), where the conducting vessels are homogeneously distributed in the annual ring structure (40). Freshly cut, well-hydrated branches are connected at one end to a pressure sensor and sealed at the other end to create a closed vascular system (Fig. 4*A* and *Materials and Methods*).

First, we observe that bending generates a large increase of the water pressure in the xylem, hence confirming the first observations of Lopez et al. (23) (Fig. 4*B*). The overpressure is independent of the bending rate or bending history (Fig. 4*C*), indicating a reversible response as in the case of the biomimetic branches. Second, for all branches and species studied, we again recover a quadratic relationship between the overpressure and the bending strain (Fig. 4*D*), once the pressure ΔP^* and the bending strain ε_B^* are properly defined to take into account dead-volume effects and the rest natural curvature of the branches (see *Extension of the Model to Beams with a Rest Curvature*, Fig. S3, and ref. 41 for the generalization of the model to naturally curved branches). The amplitude of the response for a given strain also strongly depends on the species or growing conditions, in addition to large intraspecific dispersions. By fitting the averaged data for each species and growing conditions by a quadratic law $\Delta P^* = a \times {\varepsilon_B^*}^2$, we found a clear positive correlation between the amplitude factor a and the longitudinal Young's modulus $E_\parallel$ of the branches (Fig. 4*E*). The case of *P. alba* × *tremula* L. is especially instructive. Although all branches come from the same inbred line, the hydraulic pulse induced by bending is much higher in trees grown outside, which show much stiffer mechanical properties (red symbols in Fig. 4 *D* and *E*), than trees grown indoor, which show softer properties (black symbols in Fig. 4 *D* and *E*). This is a strong indication that elasticity, like in the biomimetic systems, controls the generation of the hydraulic pulse in natural branches.

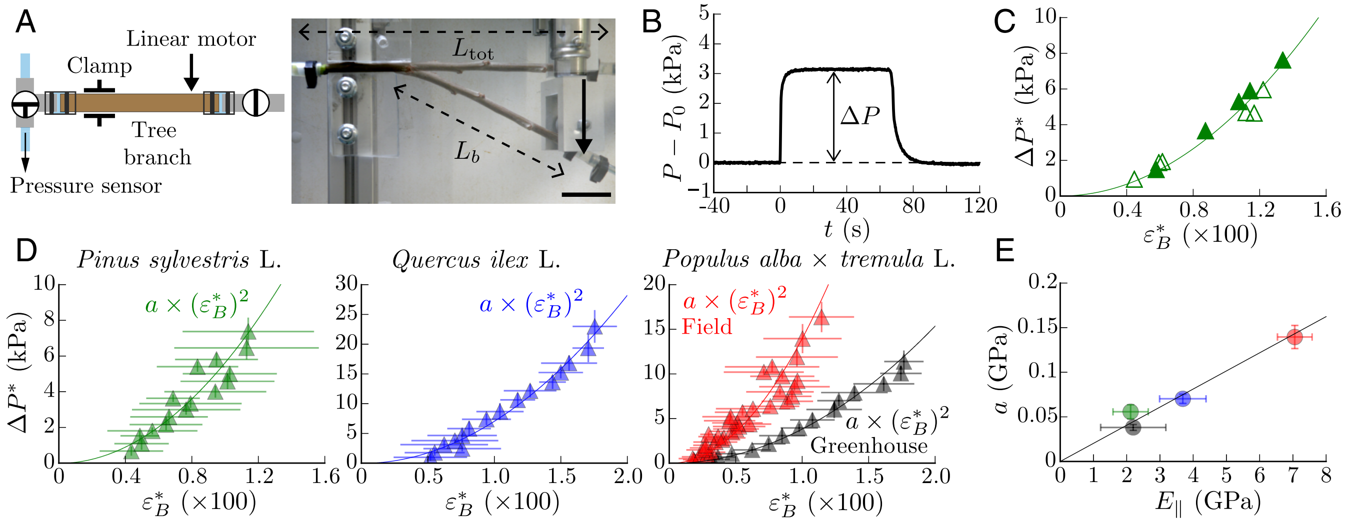

Fig. 4. Hydraulic pulse induced by bending in natural tree branches. (*A*) Sketch of the experimental setup, where L_{tot} is the total branch length and L_b the bent length. (Scale bar, 5 cm.) (*B*) Xylem water pressure measured at the fixed extremity of a pine branch (*Pinus sylvestris* L.) in response to a bent/unbent sequence. (*C*) Relationship between the overpressure and the bending strain for the same branch using two different bending protocols: incremental step displacement (filled symbols) and step displacement with return to the initial position after each bending (open symbols). Here, $\Delta P^* = \Delta P \times (L_{\text{tot}}/L_b)$ and $\varepsilon_B^* = \varepsilon_B(1+\varepsilon_B^0/\varepsilon_B)^{1/2}$, where $\varepsilon_B = R(\overline{C}-\overline{C}^0)$ and $\varepsilon_B^0 = R\overline{C}^0$, with $\overline{C}^0$ the mean curvature of the branch at rest (*Extension of the Model to Beams with a Rest Curvature*). The solid line is a quadratic fit of the data. (*D*) Overpressure ΔP^* vs. bending strain ε_B^* averaged over n branches for different tree species and growing conditions (symbols) with quadratic fit $a \times {\varepsilon_B^*}^2$ (solid lines). Green: *P. sylvestris* L., $n=6$, $a = 0.056 \pm 0.008$ GPa, $R^2 = 0.91$; blue: *Q. ilex* L., $n=5$, $a = 0.070 \pm 0.005$ GPa, $R^2 = 0.94$; red: *Populus alba* × *tremula* L. grown in field condition, $n=7$, $a = 0.139 \pm 0.013$ GPa, $R^2 = 0.88$; black: *P. alba* × *tremula* L. grown in greenhouse conditions, $n=4$, $a = 0.038 \pm 0.003$ GPa, $R^2 = 0.98$). Each symbol corresponds to a running average over five data (seven data for poplar in field conditions) with an overlap of 50%; error bars give the SD. (*E*) Coefficient of the quadratic fit a as function of the longitudinal Young's modulus $E_\parallel$ (same color as in *D*). The coefficient a is found proportional to $E_\parallel$ (solid line: linear fit, $R^2 = 0.96$).

Comparison Between the Natural and Biomimetic Systems. To further investigate the similarity between the synthetic and biological branches, we gather in the Fig. 5 *Inset* the pressure response obtained in all systems as a function of the bending strain. As expected, for a given strain, the amplitude of the pressure pulse is almost three orders of magnitude larger in the natural woody branches, whose Young's moduli are of the order of a few gigapascals, than in the soft synthetic branches, whose Young's moduli are of the order of a few megapascals. More precisely, the model predicts that the relevant parameters controlling the response should be the elastic bulk modulus B of the porous beam. Such mechanical property is difficult to measure or compute in natural branches, as it would require the knowledge of both the anatomy of the conductive network and the transverse elastic properties of the wood. However, we are able to obtain reliable measurements on the poplar branches grown outdoors, giving $B = 0.37 \pm 0.08$ GPa, that is $B \simeq E_\parallel/18$ (*Materials and Methods*, *Measurement of the Elastic Bulk Modulus in Woody Branches*, and Fig. S4). The bulk modulus of the other species or other growing condition is then estimated from their longitudinal Young modulus by assuming the same relationship to hold. Remarkably, when the pressure response is normalized by the value of the elastic bulk modulus of each branch, data from the biomimetic and biological systems all collapse on the same master quadratic curve over a range of 5 decades (Fig. 5). The prefactor of the law $\gamma \simeq 0.50 \pm 0.01$ is also compatible with the model prediction. This latter observation may appear surprising, as the model was built for isotropic elastic materials, while wood is highly anisotropic (orthotropic) (33, 34). A crude generalization of the energy model for orthotropic media gives: $\Delta P = B(E_\parallel/4E_\perp)(1-\nu_\perp)/\psi \times \varepsilon_B^2$, where $E_\perp$ is the Young's modulus in the transverse direction, $\nu_\perp$ is an effective 2D transverse Poisson's ratio, and ψ is the volume fraction of the conductive channels (see *Energy Model for Anisotropic Beams*). Our results on natural tree branches showing that $\Delta P/B \sim \varepsilon_B^2$ therefore suggest that $(E_\parallel/4E_\perp)(1-\nu_\perp)/\psi \sim 1$, compatible with mechanical properties of green woods in a wide range of tree species ($E_\parallel \sim 10E_\perp$, $\nu_\perp \sim 0.6$, $\psi \sim 0.5$) (33, 42). Interestingly, our prediction can also be compared with the experiments of Lopez et al. that reported hydraulic pulses in other tree species (23). In their study, they bent branches open at both ends and systematically measured the flux of water expelled during bending increments. We reanalyze their data to extract the total amount of water expelled $\Delta V_c/V_c$ as a function of the bending deformation ε_B. Although the species and experimental protocol (open vs. closed system) differ from our study, their data are found to follow the quadratic law predicted by our mechanism [*Revisiting Lopez et al. (2014)* and Fig. S5]. The prefactor of the quadratic law is also of order one, which gives another independent measure that fulfills the relationship $(E_\parallel/4E_\perp)(1-\nu_\perp)/\psi \sim 1$ in woody branches.

Discussion

Hydraulic pulses induced by bending were recently put forward as a promising pathway for the rapid transmission of mechanosensing information in plants. However, how such signals could be physically generated, and how they rely on the biomechanical traits of plant tissues remained poorly understood. In this work, we address these issues using a biomimetic approach. We reveal a generic mechanism for the generation of hydraulic pressure pulses under bending, both in soft artificial branches and natural tree branches. Our mechanism relies on a nonlinear coupling between the bending and transverse mode of deformation of the beam that squeezes its cross-section, by analogy with the ovalization of thin, hollow tubes. This flattening then induces a global increase of the hydraulic pressure in the conductive channels of the branch that varies quadratically with the bending strain. Hence, unlike predictions of the linear beam theory, a nonzero hydraulic pressure pulse can be produced under bending in a poroelastic beam due to nonlinear

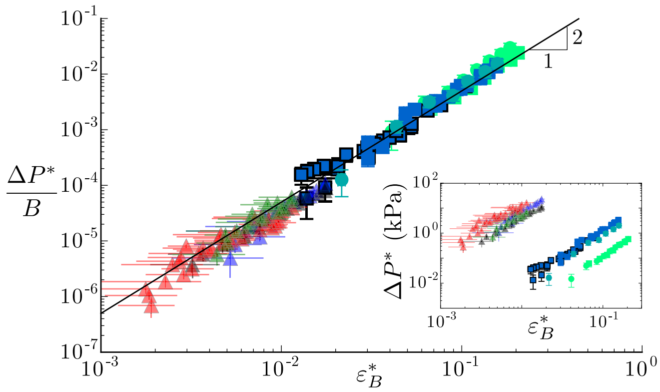

Fig. 5. Comparison between biomimetic (squares; same symbols as in Fig. 3) and natural tree branches (triangles; same symbols as in Fig. 4). The overpressure ΔP^* normalized by the elastic bulk modulus B of each branch shows a common behavior with the amplitude of the bending strain ε_B^*. The solid line represents the best quadratic fit of all data in log–log scale: $\Delta P^*/B = (0.50 \pm 0.01) \times {\varepsilon_B^*}^2$ ($R^2 = 0.98$). (*Inset*) Overpressure vs. bending strain for all data.

geometrical effects, independent of the material properties. This finding confirms and explains the paradox previously hypothesized about the origin of hydraulic pulses induced by bending in plants (23). In an engineering context, it could also be applied to artificial devices like microfluidic pumps or soft robots to rectify pressure and fluid flow under oscillatory motion (32, 43).

The simple poroelastic model we built shows that the key parameter controlling the amplitude of the pressure response is the elastic bulk modulus of the branch, a mechanical property that mainly depends on the Young's modulus of the branch. The master curve that enlightens a unique mechanical law for artificial and natural branches is available in a wide range of material rigidities (Fig. 5), suggesting the robustness of the theoretical modeling. The few key parameters that drive the generation of the hydraulic pulse are basic patterns, which are common to all plants: the presence of a conducting hydraulic network in a rigid structure, without any further prerequisites about the other structural parameters. This suggests a universal physical phenomenon that occurs in all plants that daily experience the mechanical loads of the wind (44).

Our study therefore gives a physical basis for long-distance communication in plants based on hydraulic signals. However, for these pressure pulses to function as information carriers, they must fulfill two main conditions: (*i*) they should transfer rapidly information from the places that experience the mechanical stimuli to the apical zones that sense the signal; and (*ii*) they should be perceived and converted to a relevant physiological response (thigmomorphogenetic growth response).

According to our study, a bending strain of few percent caused by wind sway (44) generates a hydraulic pressure pulse of amplitude 0.01–0.1 MPa without change of conductivity (the squeezing of the cross-section is of order $\sim 10^{-4}$). This pressure pulse first propagates ballistically at the speed of the compressive elastic waves $c = \sqrt{B/\rho} \simeq 500$ m s^{-1} (ρ is the water density) (45), then spreads with a diffusive dynamics when viscous effects prevail over inertia. This cross-over between the ballistic and diffusive regime naturally defines an effective range L_b of propagation without damping when the inertial timescale $\tau_i \sim L_b/c$ becomes equal to the poroelastic timescale $\tau_p \sim L_b^2/\mathcal{D}$ (25), where $\mathcal{D} \sim d^2 B/\eta$ is a longitudinal diffusion coefficient related to the channels diameter d, the channel elasticity B, and the water viscosity η. Typical values for woody tissues give $L_b \sim \mathcal{D}/c \sim 1$ m ($d \sim 50$ µm, $B \sim 0.3$ GPa, $\eta \sim 1$ mPa s). Beyond this length, the hydraulic signal still propagates rapidly, but with a diffusive dynamics (the effective speed of the diffusion front $\mathcal{D}/L$ is about 50 m s^{-1} for a traveling distance $L = 10$ m).

Even though hydraulic pulses spread rapidly throughout the conductive network, whether they are perceived or not as a signal is still an open question. Typical pressure pulses induced by bending are one order of magnitude smaller in amplitude than the slow daily variation of the (negative) water pressure in the conductive network of transpiring plants (35), but their frequency is much higher (typically a few hertz). This separation of amplitude and time scales is found in most biological sensory systems (46). How this overpressure may be sensed in the apical part is still under debate, but recent works suggest that mechanosensing channels could be involved in this transduction process (11, 12), opening the pathway for ion fluxes that generate local electrical signals and molecular responses (16). Future works are needed to address these issues and establish whether thigmomorphogenesis in plants do rely on this peculiar mode of signaling: hydraulics.

Materials and Methods

Experiments on Biomimetic Branches. Synthetic branches are made in PDMS with the Sylgard 184 Silicone Elastomer Kit using either 10% or 4% (wt) cross-linker (degassed for 30 min). The liquid PDMS is injected in a negative 3D mold made of a poly(methyl methacrylate) (PMMA) tube (length $L = 10$ cm, inner diameter $D = 1$ cm) containing piano strings (diameter $d = 500$ µm) fixed at both extremities in a pattern of holes drilled in a polyoxymethylene (POM) plate. Once cured (1 wk at 60 °C), the solid PDMS beam is removed from the mold and fitted into two perforated PMMA blocks. The channels are then filled with a viscous silicone oil (viscosity 1 Pa·s) and connected together to a differential pressure sensor. The Young's modulus E of the beam's matrix is determined from plain slender rods of PDMS by using a tensile testing device in the linear regime of deformation (<25%). The elastic bulk modulus B of the synthetic branches is determined by injecting a given amount of liquid inside the channels with a microsyringe and measuring the corresponding increase of liquid pressure. The beams are bent either manually or by using an automated bending device (see *Bending Setup for the Biomimetic Branches* for details). The mean curvature of the beam is measured from the difference of the angle of the beam's profile at both extremities.

Experiments with Plant Materials. All experiments are conducted between May and September on well-watered trees (see *Plant Materials* for details on the species and growing conditions). Buds and leaves are removed a few days before collecting the materials, and the scars are glued to avoid leaks during measurements. The cutting of branches and stems is done following the method described in ref. 47 to avoid any air contamination in the conducting system. The branches are then plugged to the experimental setup and flushed for several hours with degassed water to fill the conductive hydraulic network. During the bending, the branches are either in air or immersed in water to avoid evaporation. The determination of the longitudinal Young's modulus $E_\parallel$ of the branches is done after each experiment by using a standard four-point bending test. The determination of the elastic bulk modulus B of the channels is done by applying pressure increments ΔP to the water-saturated xylem of the branch (*Measurement of the Elastic Bulk Modulus in Woody Branches*).

Refined Model. In the *Results*, the quadratic relationship [**1**] between the hydraulic overpressure ΔP and the bending strain ε_B is obtained from simple scaling arguments, assuming a uniform transverse strain $\varepsilon_\perp \sim \delta/R$ in the cross-section of the beam. Here, the prefactor γ of the scaling law is computed by taking into account the spatial variation of the transverse strain. For a cylindrical elastic beam of radius R, bent with a uniform curvature C, the balance of the bending longitudinal stress implies the existence of a compressive stress in the transverse direction due to the finite curvature of the beam. This second-order effect in the slender beam parameter RC is responsible for the ovalization of the cross-section and gives rise to a parabolic transverse strain field given by ref. 48:

$$\varepsilon_\perp(z) = \frac{1}{3}\left[1 - \left(\frac{z}{R}\right)^2\right] \times \varepsilon_B^2, \qquad [2]$$

where $\varepsilon_B = RC$ and z is the height from the neutral line. To compute the liquid overpressure ΔP_i generated by this transverse compression field in the i^{th} channel, a mean field approach is used in the limit of low channel density (low porosity). Each channel at height z_i filled with an incompressible fluid is assumed to deform as if it was isolated in an effective infinite elastic medium and subjected to an external uniform compression field $\varepsilon_\perp(z_i)$. By using the superposition principle, the relative change of volume Δv_i of each channel is then given by the sum of the volume variation induced by the transverse compression strain $\varepsilon_\perp(z_i)$ and by the overpressure ΔP_i (see ref. 36, chapter 13, problem 5, and chapter 7, problem 4); that is:

$$\frac{\Delta v_i}{v_i} = -2 \times \varepsilon_\perp(z_i) + \frac{\Delta P_i}{B_i}, \qquad \textbf{[3]}$$

where v_i is the channel volume and B_i is the channel bulk modulus as defined in the *Results*. In a closed system, the incompressibility of the liquid implies $\sum_i \Delta v_i = 0$. Moreover, in natural branches and in our experiments, the channels are always interconnected hydraulically, so the overpressure is uniform ($\Delta P_i = \Delta P$). Therefore, substituting Eq. **2** in Eq. **3** and summing over all channels for identical channels ($B_i = B$ and $v_i = v$) gives Eq. **1** with:

$$\gamma = \frac{2}{3N}\sum_{i=1}^{N}\left[1 - \left(\frac{z_i}{R}\right)^2\right], \qquad \textbf{[4]}$$

where N is the number of channels.

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